# Exact solution of pulled, directed vesicles with sticky walls in two dimensions

#### Aleks Owczarek<sup>1</sup> and **Thomas Prellberg**<sup>2</sup>

<sup>1</sup>School of Mathematics and Statistics The University of Melbourne, Australia

<sup>2</sup>School of Mathematical Sciences Queen Mary University of London, UK

Open Statistical Physics Milton Keynes, March 2019

イロト 不得 トイヨト イヨト









3 Exact Solution and Phase Diagram

= nar

• Vesicles: closed membranes formed of lipid bi-layers



nan

• Vesicles commercially produced by electro-swelling



イロト イボト イヨト イヨト

990

Э

• Red blood cells: lipid bi-layer + spectrin network



イロト イヨト イヨト

5990

• Red blood cells: effect of osmotic pressure



<ロト < 回 > < 回 > < 回 > < 回 >

э 590

• Red blood cells pulled with optical tweezer









イロト イボト イヨト イヨト

590

Э







## Modelling Vesicles

We model vesicles as two-dimensional self-avoiding polygons.



Figure: A self-avoiding polygon of perimeter 2n = 52 and area a = 37.

イロト イヨト イヨト

The Vesicle Generating Function

$$G(q,t) = \sum_{n,a} c_{n,a} t^n q^a$$

where  $c_{n,a}$  is the number of SAP with perimeter 2*n* and area *a*.

イロト イポト イヨト イヨト

nac

The Vesicle Generating Function

$$G(q,t) = \sum_{n,a} c_{n,a} t^n q^a$$

where  $c_{n,a}$  is the number of SAP with perimeter 2n and area a.



Thomas Prellberg(QMUL) Pulled vesicles

## Pulled Directed Sticky Vesicles (PDSV)

- Red blood cell shape pprox preferred direction
- Membrane defects  $\approx$  sticky contacts
- $\bullet$  Optical tweezer  $\approx$  pulling force

イロト イポト イヨト イヨト

## Pulled Directed Sticky Vesicles (PDSV)

- Red blood cell shape  $\approx$  preferred direction
- Membrane defects  $\approx$  sticky contacts
- Optical tweezer  $\approx$  pulling force



Figure: Two directed walks representing a vesicle with perimeter 2n = 24 and area a = 8, with number of contacts m = 4, and indicated pulling force.

イロト イヨト イヨト

The PDSV Generating Function

$$F(c, x, y, q) = \sum_{n_x, n_y, a, m} c_{n_x, n_y, a, m} x^{n_x} y^{n_y} q^a c^m$$

where  $c_{n_x,n_y,a,m}$  is the number of PDSV with  $n_x$  SE steps,  $n_y$  NE steps, area *a*, and *m* contacts.



イロト イヨト イヨト

The PDSV Generating Function

$$F(c, x, y, q) = \sum_{n_x, n_y, a, m} c_{n_x, n_y, a, m} x^{n_x} y^{n_y} q^a c^m$$

where  $c_{n_x,n_y,a,m}$  is the number of PDSV with  $n_x$  SE steps,  $n_y$  NE steps, area *a*, and *m* contacts.



The vertical *endpoint displacement* is given by  $h = n_y - n_x$ , so introduce the variable  $s = e^{-\beta h f}$  conjugate to a *pulling force* f:

$$G(c,s,q,t) = \sum_{m,h,n,a} c_{n_x,n_y,a,m} t^{n_x+n_y} s^{n_y-n_x} q^a c^m = F(c,t/s,ts,q)$$

イロト 不同 トイヨト イヨト

## **Exact Solution**

$$F(c, x, y, q) = \frac{1}{1 - cx - \frac{cy}{1 + y - qx - \frac{y}{1 + y - q^2x - \frac{y}{1 + y - q^3x - \dots}}}$$
$$= \frac{1}{1 - c \left[ x + y \frac{\sum_{n=0}^{\infty} \frac{(-q^2x)^n q^{\binom{n}{2}}}{(q; q)_n (qy; q)_n}}{\sum_{n=0}^{\infty} \frac{(-qx)^n q^{\binom{n}{2}}}{(q; q)_n (qy; q)_n}} \right]$$
where  $(t; q)_n = \prod_{k=0}^{n-1} (1 - tq^k)$ .

・ロト ・回 ト ・ヨト ・ヨト

Ξ 9 Q (?

#### The PDSV Generating Function for q = 1

Singularity  $t_c(c, s, q = 1)$  of G(c, s, q = 1, t):



- **unbound** and **bound** phases
- phase transition at

$$c_s = \frac{(s+1)^2}{s^2+s+1}$$

イロト イポト イヨト イヨト

nan

## The PDSV Generating Function for q = 1

Singularity  $t_c(c, s, q = 1)$  of G(c, s, q = 1, t):



- **unbound** and **bound** phases
- phase transition at

$$c_s=\frac{(s+1)^2}{s^2+s+1}$$

-

ヨート

Density of contacts

$$\mathcal{M}(c,s,q=1) = egin{cases} 0\,, & c \leq c_{s} \ \sim rac{2}{c_{s}^{2}}rac{(1+s)^{2}}{s}(c-c_{s})\,, & c > c_{s} \end{cases}$$

#### The PDSV Phase Diagram for q = 1



- unbound and bound phases
- The transition looks sharper when decreasing *s* to zero, but is still smooth

イロト イボト イヨト イヨト

Э

• symmetry between f and -f implies invariance  $s \rightarrow 1/s$ 

## The PDSV Generating Function for $q \neq 1$

- q > 1: The bound phase disappears
  - Configurations with large area  $a \sim n^2$  dominate, so  $t_c = 0$
- q < 1: The unbound phase disappears
  - $\bullet\,$  The density of contacts is positive for any values of s and c

◆□▶ ◆□▶ ◆三▶ ◆三▶ 三三 - シスペ

## The PDSV Generating Function for $q \neq 1$

- q > 1: The bound phase disappears
  - Configurations with large area  $a \sim n^2$  dominate, so  $t_c = 0$
- q < 1: The unbound phase disappears
  - $\bullet\,$  The density of contacts is positive for any values of s and c
- Singularity  $t_c(c, s = 1, q)$  of G(c, s = 1, q, t):



• Smooth function of c when q < 1

イロト イヨト イヨト

• Critical point at q = 1 and c = 4/3

## The PDSV Generating Function for $q \neq 1$

- q > 1: The bound phase disappears
  - Configurations with large area  $a \sim n^2$  dominate, so  $t_c = 0$
- q < 1: The unbound phase disappears
  - $\bullet\,$  The density of contacts is positive for any values of s and c
- Singularity  $t_c(c, s = 1, q)$  of G(c, s = 1, q, t):



• Smooth function of c when q < 1

◆□▶ ◆□▶ ◆三▶ ◆三▶ 三三 - シスペ

• Critical point at q = 1 and c = 4/3

• No structural difference upon changing s, keep s = 1 from now on

### Scaling Around the Critical Point

• Near the critical point at q = 1 and c = 4/3 we find a scaling form

$$c \sim \frac{1}{\frac{3}{4} + 4^{-2/3} \epsilon^{1/3} \frac{\mathsf{Ai}'(4^{1/3}(1 - 4t_c)\epsilon^{-2/3})}{\mathsf{Ai}(4^{1/3}(1 - 4t_c)\epsilon^{-2/3})}}$$

with  $\epsilon = 1 - q$ , where Ai(z) is the Airy function.

◆□▶ ◆□▶ ◆三▶ ◆三▶ 三三 - シスペ

## Scaling Around the Critical Point

• Near the critical point at q = 1 and c = 4/3 we find a scaling form

$$c \sim \frac{1}{\frac{3}{4} + 4^{-2/3} \epsilon^{1/3} \frac{\mathsf{Ai}'(4^{1/3}(1 - 4t_c)\epsilon^{-2/3})}{\mathsf{Ai}(4^{1/3}(1 - 4t_c)\epsilon^{-2/3})}}$$

with  $\epsilon = 1 - q$ , where Ai(z) is the Airy function.

• For c = 4/3, and  $a'_1 = -1.0187...$  the first zero of Ai'(z):

- The singularity  $t_c$  approaches 1/4 as  $t_c \sim rac{1}{4} a_1' 4^{-4/3} \epsilon^{2/3}$
- The average area diverges as

$$\mathcal{A}\sim -a_1^\prime \frac{2^{1/3}}{3} \epsilon^{-1/3}$$

• The density of contacts vanishes as

$$\mathcal{M} \sim -rac{1}{a_1'} rac{3}{4^{2/3}} \epsilon^{1/3}$$



#### The PDSV Phase Diagram



#### The PDSV Phase Diagram

