

Appendix

A.1. Vector identities

$$(\mathbf{a} \wedge \mathbf{b}) \wedge \mathbf{c} = (\mathbf{a} \cdot \mathbf{c})\mathbf{b} - (\mathbf{b} \cdot \mathbf{c})\mathbf{a}, \quad (\text{A.1})$$

$$\nabla \wedge \nabla \phi = 0, \quad \nabla \cdot (\nabla \wedge \mathbf{F}) = 0, \quad (\text{A.2, A.3})$$

$$\nabla \cdot (\phi \mathbf{F}) = \phi \nabla \cdot \mathbf{F} + \mathbf{F} \cdot \nabla \phi, \quad (\text{A.4})$$

$$\nabla \wedge (\phi \mathbf{F}) = \phi \nabla \wedge \mathbf{F} + (\nabla \phi) \wedge \mathbf{F}, \quad (\text{A.5})$$

$$\nabla \wedge (\mathbf{F} \wedge \mathbf{G}) = (\mathbf{G} \cdot \nabla)\mathbf{F} - (\mathbf{F} \cdot \nabla)\mathbf{G} + \mathbf{F}(\nabla \cdot \mathbf{G}) - \mathbf{G}(\nabla \cdot \mathbf{F}), \quad (\text{A.6})$$

$$\nabla \cdot (\mathbf{F} \wedge \mathbf{G}) = \mathbf{G} \cdot (\nabla \wedge \mathbf{F}) - \mathbf{F} \cdot (\nabla \wedge \mathbf{G}), \quad (\text{A.7})$$

$$\nabla(\mathbf{F} \cdot \mathbf{G}) = \mathbf{F} \wedge (\nabla \wedge \mathbf{G}) + \mathbf{G} \wedge (\nabla \wedge \mathbf{F}) + (\mathbf{F} \cdot \nabla)\mathbf{G} + (\mathbf{G} \cdot \nabla)\mathbf{F}, \quad (\text{A.8})$$

$$(\mathbf{F} \cdot \nabla)\mathbf{F} = (\nabla \wedge \mathbf{F}) \wedge \mathbf{F} + \nabla(\frac{1}{2}F^2), \quad (\text{A.9})$$

$$\nabla^2 \mathbf{F} = \nabla(\nabla \cdot \mathbf{F}) - \nabla \wedge (\nabla \wedge \mathbf{F}). \quad (\text{A.10})$$

A.2. Two properties of the gradient operator ∇

Let $\phi(\mathbf{x})$ be some scalar function of \mathbf{x} , and let $d\phi/ds$ be its rate of change, with distance s , in the direction of some unit vector \mathbf{t} . Then

$$d\phi/ds = \mathbf{t} \cdot \nabla \phi. \quad (\text{A.11})$$

For this very reason, the line integral of $\nabla \phi$ along some curve C is equal to the difference in ϕ between the two end-points of the curve:

$$\int_C \nabla \phi \cdot d\mathbf{x} = [\phi]_C. \quad (\text{A.12})$$

A.3. The divergence theorem

Let the region V be bounded by a simple closed surface S with unit outward normal \mathbf{n} . Then

$$\int_S \mathbf{F} \cdot \mathbf{n} \, dS = \int_V \nabla \cdot \mathbf{F} \, dV. \quad (\text{A.13})$$

In suffix notation, and using the summation convention, this takes the form

$$\int_S F_j n_j \, dS = \int_V \frac{\partial F_j}{\partial x_j} \, dV.$$

There are many identities which may be derived from the divergence theorem. The identity

$$\int_S \phi \mathbf{n} \, dS = \int_V \nabla \phi \, dV \quad (\text{A.14})$$

is particularly valuable, and may be written

$$\int_S \phi n_j \, dS = \int_V \frac{\partial \phi}{\partial x_j} \, dV. \quad (\text{A.15})$$

The following are immediate consequences:

$$\int_S F_j n_j \, dS = \int_V \frac{\partial F_j}{\partial x_j} \, dV, \quad \int_S T_{ij} n_j \, dS = \int_V \frac{\partial T_{ij}}{\partial x_j} \, dV, \quad (\text{A.16, A.17})$$

$$\int_S u_i v_j n_j \, dS = \int_V \frac{\partial}{\partial x_j} (u_i v_j) \, dV. \quad (\text{A.18})$$

Other identities derivable from the divergence theorem include:

$$\int_S \mathbf{F} \wedge \mathbf{n} \, dS = - \int_V \nabla \wedge \mathbf{F} \, dV, \quad \int_S \mathbf{n} \cdot \nabla \phi \, dS = \int_V \nabla^2 \phi \, dV, \quad (\text{A.19, A.20})$$

$$\int_S \phi \frac{\partial \psi}{\partial n} \, dS = \int_V (\phi \nabla^2 \psi + \nabla \phi \cdot \nabla \psi) \, dV, \quad (\text{A.21})$$

$$\int_S \left(\phi \frac{\partial \psi}{\partial n} - \psi \frac{\partial \phi}{\partial n} \right) \, dS = \int_V (\phi \nabla^2 \psi - \psi \nabla^2 \phi) \, dV. \quad (\text{A.22})$$

A.4. Stokes's theorem

Let C be a simple closed curve spanned by a surface S with unit normal \mathbf{n} . Then

$$\int_C \mathbf{F} \cdot d\mathbf{x} = \int_S (\nabla \wedge \mathbf{F}) \cdot \mathbf{n} \, dS, \quad (\text{A.23})$$

where the line integral is taken in an appropriate sense, according to that of \mathbf{n} (see Fig. A.1).

Green's theorem in the plane may be viewed as a special case of Stokes's theorem, with $\mathbf{F} = [u(x, y), v(x, y), 0]$. If C is a simple closed curve in the x - y plane, and S denotes the region enclosed by C , then

$$\int_C u \, dx + v \, dy = \int_S \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) dx \, dy. \quad (\text{A.24})$$

A useful identity derivable from Stokes's theorem is

$$\int_C \phi \, dx = - \int_S (\nabla \phi) \wedge \mathbf{n} \, dS. \quad (\text{A.25})$$

A.5. Orthogonal curvilinear coordinates

Let u , v , and w denote a set of orthogonal curvilinear coordinates, and let \mathbf{e}_u , \mathbf{e}_v and \mathbf{e}_w denote unit vectors parallel to the coordinate lines and in the directions of increase of u , v , and w respectively. Then

$$\mathbf{e}_u = \mathbf{e}_v \wedge \mathbf{e}_w, \quad \text{etc.},$$

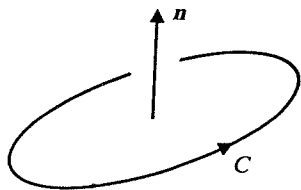


Fig. A.1.

and

$$\delta \mathbf{x} = h_1 \delta u \mathbf{e}_u + h_2 \delta v \mathbf{e}_v + h_3 \delta w \mathbf{e}_w,$$

where

$$h_1 = |\partial \mathbf{x} / \partial u|, \quad \text{etc.}$$

Furthermore,

$$\nabla \phi = \frac{1}{h_1} \frac{\partial \phi}{\partial u} \mathbf{e}_u + \frac{1}{h_2} \frac{\partial \phi}{\partial v} \mathbf{e}_v + \frac{1}{h_3} \frac{\partial \phi}{\partial w} \mathbf{e}_w, \quad (\text{A.26})$$

$$\nabla \cdot \mathbf{F} = \frac{1}{h_1 h_2 h_3} \left[\frac{\partial}{\partial u} (h_2 h_3 F_u) + \frac{\partial}{\partial v} (h_3 h_1 F_v) + \frac{\partial}{\partial w} (h_1 h_2 F_w) \right], \quad (\text{A.27})$$

$$\nabla \wedge \mathbf{F} = \frac{1}{h_1 h_2 h_3} \begin{vmatrix} h_1 \mathbf{e}_u & h_2 \mathbf{e}_v & h_3 \mathbf{e}_w \\ \frac{\partial}{\partial u} & \frac{\partial}{\partial v} & \frac{\partial}{\partial w} \\ h_1 F_u & h_2 F_v & h_3 F_w \end{vmatrix}. \quad (\text{A.28})$$

For cylindrical polar coordinates (Fig. A.2)

$$\begin{aligned} u = r, & \quad v = \theta, & \quad w = z, \\ h_1 = 1, & \quad h_2 = r, & \quad h_3 = 1. \end{aligned}$$

For spherical polar coordinates (Fig. A.3)

$$\begin{aligned} u = r, & \quad v = \theta, & \quad w = \phi, \\ h_1 = 1, & \quad h_2 = r, & \quad h_3 = r \sin \theta. \end{aligned}$$

A.6. Cylindrical polar coordinates

Cylindrical polar coordinates (r, θ, z) are such that

$$x_1 = r \cos \theta, \quad x_2 = r \sin \theta, \quad x_3 = z,$$

as in Fig. A.2. Clearly,

$$\delta \mathbf{x} = \delta r \mathbf{e}_r + r \delta \theta \mathbf{e}_\theta + \delta z \mathbf{e}_z$$

and

$$\mathbf{e}_r = \cos \theta \mathbf{e}_1 + \sin \theta \mathbf{e}_2, \quad \mathbf{e}_\theta = -\sin \theta \mathbf{e}_1 + \cos \theta \mathbf{e}_2, \quad \mathbf{e}_z = \mathbf{e}_3.$$

The unit vectors do not change with r or z , but

$$\frac{\partial \mathbf{e}_r}{\partial \theta} = \mathbf{e}_\theta, \quad \frac{\partial \mathbf{e}_\theta}{\partial \theta} = -\mathbf{e}_r, \quad \frac{\partial \mathbf{e}_z}{\partial \theta} = 0. \quad (\text{A.29})$$

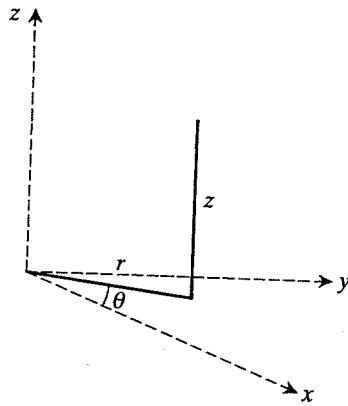


Fig. A.2 Cylindrical polar coordinates.

Also,

$$\nabla\phi = \frac{\partial\phi}{\partial r}e_r + \frac{1}{r}\frac{\partial\phi}{\partial\theta}e_\theta + \frac{\partial\phi}{\partial z}e_z, \quad (\text{A.30})$$

$$\nabla \cdot \mathbf{F} = \frac{1}{r}\frac{\partial}{\partial r}(rF_r) + \frac{1}{r}\frac{\partial F_\theta}{\partial\theta} + \frac{\partial F_z}{\partial z}, \quad (\text{A.31})$$

$$\nabla \wedge \mathbf{F} = \frac{1}{r} \begin{vmatrix} e_r & re_\theta & e_z \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial\theta} & \frac{\partial}{\partial z} \\ F_r & rF_\theta & F_z \end{vmatrix}, \quad (\text{A.32})$$

$$\nabla^2 = \frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial}{\partial r}\right) + \frac{1}{r^2}\frac{\partial^2}{\partial\theta^2} + \frac{\partial^2}{\partial z^2}, \quad (\text{A.33})$$

$$\mathbf{u} \cdot \nabla = u_r\frac{\partial}{\partial r} + \frac{u_\theta}{r}\frac{\partial}{\partial\theta} + u_z\frac{\partial}{\partial z}. \quad (\text{A.34})$$

The Navier-Stokes equations in cylindrical polar coordinates are:

$$\begin{aligned} \frac{\partial u_r}{\partial t} + (\mathbf{u} \cdot \nabla)u_r - \frac{u_\theta^2}{r} &= -\frac{1}{\rho}\frac{\partial p}{\partial r} + \nu\left(\nabla^2 u_r - \frac{u_r}{r^2} - \frac{2}{r^2}\frac{\partial u_\theta}{\partial\theta}\right), \\ \frac{\partial u_\theta}{\partial t} + (\mathbf{u} \cdot \nabla)u_\theta + \frac{u_r u_\theta}{r} &= -\frac{1}{\rho r}\frac{\partial p}{\partial\theta} + \nu\left(\nabla^2 u_\theta + \frac{2}{r^2}\frac{\partial u_r}{\partial\theta} - \frac{u_\theta}{r^2}\right), \end{aligned} \quad (\text{A.35})$$

$$\frac{\partial u_z}{\partial t} + (\mathbf{u} \cdot \nabla)u_z = -\frac{1}{\rho}\frac{\partial p}{\partial z} + \nu\nabla^2 u_z,$$

$$\frac{1}{r}\frac{\partial}{\partial r}(ru_r) + \frac{1}{r}\frac{\partial u_\theta}{\partial\theta} + \frac{\partial u_z}{\partial z} = 0.$$

The components of the rate-of-strain tensor are given by:

$$\begin{aligned} e_{rr} &= \frac{\partial u_r}{\partial r}, & e_{\theta\theta} &= \frac{1}{r}\frac{\partial u_\theta}{\partial\theta} + \frac{u_r}{r}, & e_{zz} &= \frac{\partial u_z}{\partial z}, \\ 2e_{\theta z} &= \frac{1}{r}\frac{\partial u_z}{\partial\theta} + \frac{\partial u_\theta}{\partial z}, & 2e_{zr} &= \frac{\partial u_r}{\partial z} + \frac{\partial u_z}{\partial r}, & & \\ 2e_{r\theta} &= r\frac{\partial}{\partial r}\left(\frac{u_\theta}{r}\right) + \frac{1}{r}\frac{\partial u_r}{\partial\theta}. \end{aligned} \quad (\text{A.36})$$

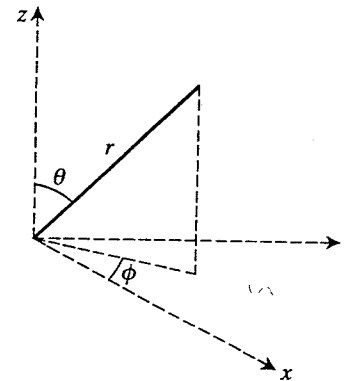


Fig. A.3. Spherical polar coordinates.

A.7. Spherical polar coordinates

Spherical polar coordinates (r, θ, ϕ) are such that

$$x_1 = r \sin \theta \cos \phi, \quad x_2 = r \sin \theta \sin \phi, \quad x_3 = r \cos \theta,$$

as in Fig. A.3. Clearly,

$$\delta \mathbf{x} = \delta r \mathbf{e}_r + r \delta \theta \mathbf{e}_\theta + r \sin \theta \delta \phi \mathbf{e}_\phi$$

and

$$\mathbf{e}_r = \sin \theta \cos \phi \mathbf{e}_1 + \sin \theta \sin \phi \mathbf{e}_2 + \cos \theta \mathbf{e}_3,$$

$$\mathbf{e}_\theta = \cos \theta \cos \phi \mathbf{e}_1 + \cos \theta \sin \phi \mathbf{e}_2 - \sin \theta \mathbf{e}_3,$$

$$\mathbf{e}_\phi = -\sin \phi \mathbf{e}_1 + \cos \phi \mathbf{e}_2.$$

The unit vectors do not change with r , but

$$\partial \mathbf{e}_r / \partial \theta = \mathbf{e}_\theta, \quad \partial \mathbf{e}_\theta / \partial \theta = -\mathbf{e}_r, \quad \partial \mathbf{e}_\phi / \partial \theta = 0,$$

$$\partial \mathbf{e}_r / \partial \phi = \sin \theta \mathbf{e}_\phi, \quad \partial \mathbf{e}_\theta / \partial \phi = \cos \theta \mathbf{e}_\phi, \quad (\text{A.37})$$

$$\partial \mathbf{e}_\phi / \partial \phi = -\sin \theta \mathbf{e}_r - \cos \theta \mathbf{e}_\theta.$$

Also,

$$\nabla \Phi = \frac{\partial \Phi}{\partial r} \mathbf{e}_r + \frac{1}{r} \frac{\partial \Phi}{\partial \theta} \mathbf{e}_\theta + \frac{1}{r \sin \theta} \frac{\partial \Phi}{\partial \phi} \mathbf{e}_\phi, \quad (\text{A.38})$$

$$\nabla \cdot \mathbf{F} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 F_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (F_\theta \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial F_\phi}{\partial \phi}, \quad (\text{A.39})$$

$$\nabla \wedge \mathbf{F} = \frac{1}{r^2 \sin \theta} \begin{vmatrix} \mathbf{e}_r & r \mathbf{e}_\theta & r \sin \theta \mathbf{e}_\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ F_r & r F_\theta & r \sin \theta F_\phi \end{vmatrix}, \quad (\text{A.40})$$

$$\nabla^2 = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2}{\partial \phi^2}, \quad (\text{A.41})$$

$$\mathbf{u} \cdot \nabla = u_r \frac{\partial}{\partial r} + \frac{u_\theta}{r} \frac{\partial}{\partial \theta} + \frac{u_\phi}{r \sin \theta} \frac{\partial}{\partial \phi}. \quad (\text{A.42})$$

The Navier–Stokes equations in spherical polar coordinates are:

$$\begin{aligned} \frac{\partial u_r}{\partial t} + (\mathbf{u} \cdot \nabla) u_r - \frac{u_\theta^2}{r} - \frac{u_\phi^2}{r} \\ = -\frac{1}{\rho} \frac{\partial p}{\partial r} + \nu \left[\nabla^2 u_r - \frac{2u_r}{r^2} - \frac{2}{r^2 \sin \theta} \frac{\partial}{\partial \theta} (u_\theta \sin \theta) - \frac{2}{r^2 \sin \theta} \frac{\partial u_\phi}{\partial \phi} \right], \end{aligned}$$

$$\begin{aligned} \frac{\partial u_\theta}{\partial t} + (\mathbf{u} \cdot \nabla) u_\theta + \frac{u_r u_\theta}{r} - \frac{u_\phi^2 \cot \theta}{r} \\ = -\frac{1}{\rho r} \frac{\partial p}{\partial \theta} + \nu \left[\nabla^2 u_\theta + \frac{2}{r^2} \frac{\partial u_r}{\partial \theta} - \frac{u_\theta}{r^2 \sin^2 \theta} - \frac{2 \cos \theta}{r^2 \sin^2 \theta} \frac{\partial u_\phi}{\partial \phi} \right], \end{aligned}$$

$$\begin{aligned} \frac{\partial u_\phi}{\partial t} + (\mathbf{u} \cdot \nabla) u_\phi + \frac{u_\phi u_r}{r} + \frac{u_\theta u_\phi \cot \theta}{r} \\ = -\frac{1}{\rho r \sin \theta} \frac{\partial p}{\partial \phi} + \nu \left[\nabla^2 u_\phi + \frac{2}{r^2 \sin \theta} \frac{\partial u_r}{\partial \phi} + \frac{2 \cos \theta}{r^2 \sin^2 \theta} \frac{\partial u_\theta}{\partial \phi} - \frac{u_\phi}{r^2 \sin^2 \theta} \right], \\ \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 u_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (u_\theta \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial u_\phi}{\partial \phi} = 0. \quad (\text{A.43}) \end{aligned}$$

The components of the rate-of-strain tensor are given by:

$$\begin{aligned} e_{rr} &= \frac{\partial u_r}{\partial r}, & e_{\theta\theta} &= \frac{1}{r} \frac{\partial u_\theta}{\partial \theta} + \frac{u_r}{r}, \\ e_{\phi\phi} &= \frac{1}{r \sin \theta} \frac{\partial u_\phi}{\partial \phi} + \frac{u_r}{r} + \frac{u_\theta \cot \theta}{r}, \\ 2e_{r\theta} &= \frac{\sin \theta}{r} \frac{\partial}{\partial \theta} \left(\frac{u_\phi}{\sin \theta} \right) + \frac{1}{r \sin \theta} \frac{\partial u_\theta}{\partial \phi}, \\ 2e_{r\phi} &= \frac{1}{r \sin \theta} \frac{\partial u_r}{\partial \phi} + r \frac{\partial}{\partial r} \left(\frac{u_\phi}{r} \right), \\ 2e_{r\theta} &= r \frac{\partial}{\partial r} \left(\frac{u_\theta}{r} \right) + \frac{1}{r} \frac{\partial u_r}{\partial \theta}. \end{aligned} \quad (\text{A.44})$$