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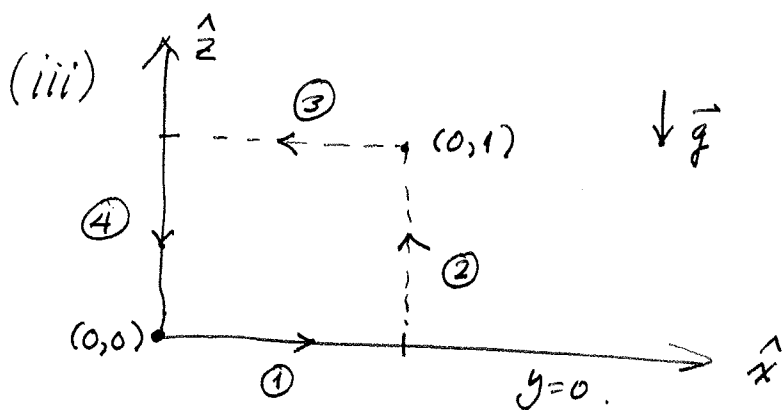
(i) $\vec{F} = m\vec{a} = m \frac{d\vec{v}}{dt} \Rightarrow m\vec{v} \cdot \frac{d\vec{v}}{dt} = \vec{F} \cdot \vec{v} = \vec{F} \cdot \frac{d\vec{r}}{dt}$

$\Rightarrow \frac{d}{dt} \left(\frac{1}{2} m \vec{v}^2 \right) = \frac{d}{dt} (KE) = \vec{F} \cdot \frac{d\vec{r}}{dt} \Rightarrow \frac{d(KE)}{dt} dt = \vec{F} \cdot \frac{d\vec{r}}{dt} dt$

$\Rightarrow d(KE) = \vec{F} \cdot d\vec{r} \equiv dW$, dW is infinitesimal work done on the object.

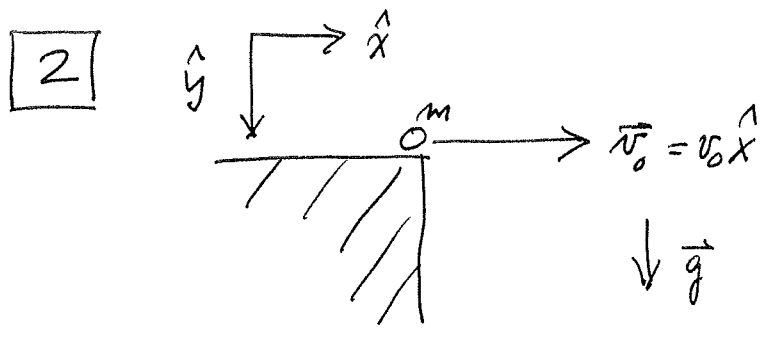
$\Rightarrow \int_1^2 d(KE) = \boxed{\int_1^2 dW = KE_2 - KE_1}$ \square .

(ii) $\Delta KE = KE_2 - KE_1 = \int_1^2 \vec{F} \cdot d\vec{r} = \int_1^2 -mg\hat{z} \cdot d\vec{r} = -mg \int_1^2 dz$
 $= -mg(z_2 - z_1) = -mg\Delta z$ \square .



$I = \oint \vec{F} \cdot d\vec{r} = \int_1 \vec{F} \cdot d\vec{x} + \int_2 \vec{F} \cdot d\vec{z} + \int_3 \vec{F} \cdot d\vec{x} + \int_4 \vec{F} \cdot d\vec{z}$,
 since $\vec{F} = -mg\hat{z}$ and $d\vec{x} = dx\hat{x}$ (i.e., $\hat{x} \perp \hat{z}$).

$\therefore I = -mg \int_0^1 dz - mg \int_1^0 dz = \boxed{0}$ \square .



(i) $-\alpha m v^2$ has the unit of force - i.e., $\frac{\text{kg m}}{\text{s}^2}$.

$$\therefore [\alpha] \text{ kg} \cdot \frac{\text{m}^2}{\text{s}^2} = \frac{\text{kg m}}{\text{s}^2} \Rightarrow \boxed{[\alpha] = \frac{1}{\text{m}}}$$

(ii) $F_x = m a_x \Rightarrow m \frac{dv_x}{dt} = -\alpha m v_x^2 \Rightarrow \boxed{\frac{dv_x}{dt} = -\alpha v_x^2}$

$$\Rightarrow \int_{v_0}^{v_x(t)} \tilde{v}_x^{-2} d\tilde{v}_x = \int_0^t -\alpha d\tilde{t} = -\alpha t = -\tilde{v}_x^{-1} \Big|_{v_0}^{v_x(t)} = \frac{1}{v_0} - \frac{1}{v_x(t)}$$

$$\Rightarrow \frac{1}{v_x(t)} = \frac{1}{v_0} + \alpha t = \frac{1 + v_0 \alpha t}{v_0} \Rightarrow \boxed{v_x(t) = \frac{v_0}{1 + v_0 \alpha t}}$$

(iii) $F_y = m a_y \Rightarrow m \frac{dv_y}{dt} = -\alpha m v_y^2 + m g \Rightarrow \boxed{\frac{dv_y}{dt} = -\alpha v_y^2 + g}$

$$\Rightarrow \int_0^{v_y(t)} \frac{d\tilde{v}_y}{g - \alpha \tilde{v}_y^2} = \int_0^t d\tilde{t} = t = \frac{\tanh^{-1}(v_y \sqrt{\frac{\alpha'}{g}})}{\sqrt{\alpha g'}}$$

using the hint.

$$\Rightarrow t \sqrt{\alpha g'} = \tanh^{-1}(v_y \sqrt{\frac{\alpha'}{g}}) \Rightarrow \tanh(\sqrt{\alpha g'} t) = v_y \sqrt{\frac{\alpha'}{g}}$$

$$\Rightarrow \boxed{v_y(t) = \sqrt{\frac{g'}{\alpha}} \cdot \tanh(\sqrt{\alpha g'} t) = \sqrt{\frac{g'}{\alpha}} \frac{e^{\sqrt{\alpha g'} t} - e^{-\sqrt{\alpha g'} t}}{e^{\sqrt{\alpha g'} t} + e^{-\sqrt{\alpha g'} t}}}$$

I.C. Check: $v_y(0) = \sqrt{\frac{g'}{\alpha}} (1-1) = 0 \checkmark$

(iv) $\sqrt{\alpha g'} t \ll 1 \Rightarrow v_y \approx \sqrt{\frac{g'}{\alpha}} \left(\frac{1 + \sqrt{\alpha g'} t - 1 + \sqrt{\alpha g'} t}{1 + \sqrt{\alpha g'} t + 1 - \sqrt{\alpha g'} t} \right)$

$$= \sqrt{\frac{g'}{\alpha}} \cdot \frac{2\sqrt{\alpha g'} t}{2} = \boxed{g t}$$

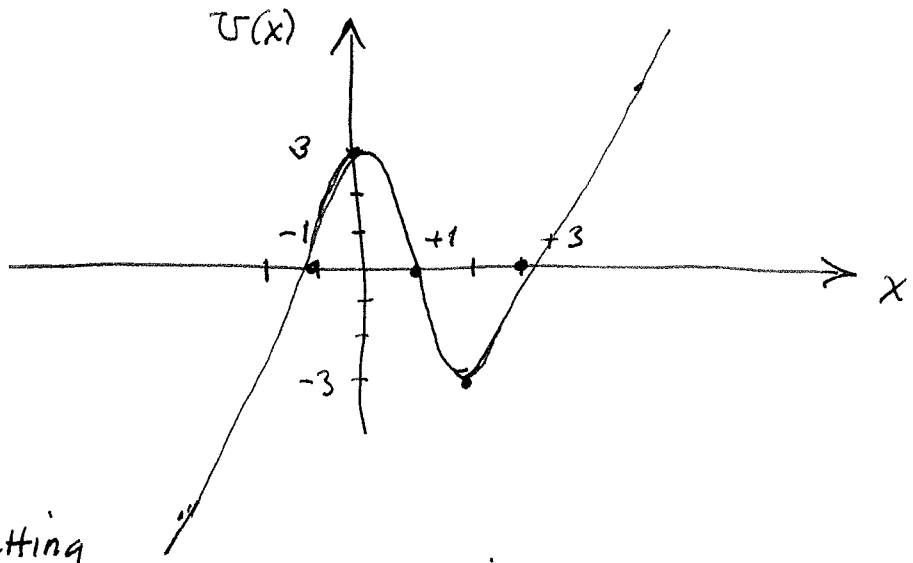
i.e., vel increase linearly with time early on.
i.e., linear, "terminal" velocity

For $t \rightarrow \infty$, we have $v_y \approx \sqrt{\frac{g'}{\alpha}} \cdot \left(\frac{1-0}{1+0} \right) = \boxed{\sqrt{\frac{g'}{\alpha}}}$

3

$$U(x) = x^3 - 3x^2 - x + 3$$

$$(i) U(x) = x^2(x-3) - (x-3) = (x^2-1) \cdot (x-3)$$



Setting

(ii) $\frac{dU}{dx} = 0$ gives the equilibrium pts $\forall x$ that satisfy the condition:

$$3x^2 - 6x - 1 = 0 \Rightarrow x_{eq} = \frac{6 \pm \sqrt{36 + 12}}{6} = 1 \pm \frac{1}{6} \sqrt{48}$$

$$x_{eq} = 1 \pm \frac{2}{3} \sqrt{3}$$

(iii) There are 2 eq. points. To see whether the pt is stable/unstable, check the 2nd - derivative of $U(x)$ at the pt:

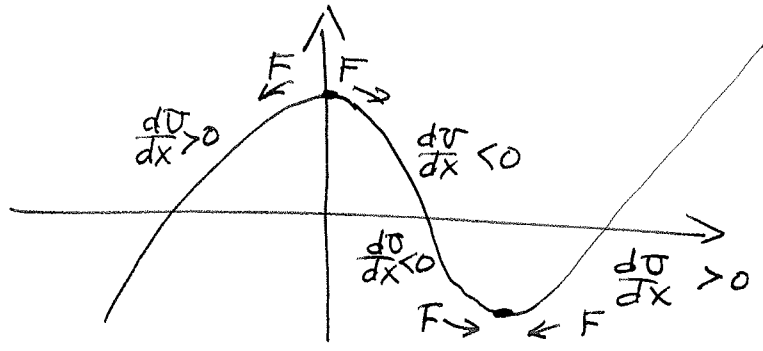
$$\frac{d^2U}{dx^2} = 6x - 6 \quad (\text{n.b., do not set this to zero. Why?})$$

$$x_{eq}^1 = 1 + \frac{2}{3} \sqrt{3} \Rightarrow \left. \frac{d^2U}{dx^2} \right|_{x_{eq}^1} = 6(1 + \frac{2}{3} \sqrt{3}) - 6 > 0. \therefore \underline{\underline{STABLE}}$$

$$x_{eq}^2 = 1 - \frac{2}{3} \sqrt{3} \Rightarrow \left. \frac{d^2U}{dx^2} \right|_{x_{eq}^2} = 6(1 - \frac{2}{3} \sqrt{3}) - 6 < 0. \therefore \underline{\underline{UNSTABLE}}$$

→ continued -

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Force = $-\frac{dU}{dx}$. \therefore Force around the eq. pts is as indicated (and, as expected).

4

(i) Given a contour loop C enclosing an area S , oriented with the normal \hat{n} , the curl of a vector field \vec{F} threading S (in the \hat{n} -direction) is equal to the line (contour) integral of \vec{F} around C (taken counter-clockwise):

$$\int_S (\nabla \times \vec{F}) \cdot \hat{n} da = \oint_C \vec{F} \cdot d\vec{r}$$

- (ii) a) The work done by the field is independent of the path taken by a particle moving in the field (i.e., the work depends only on the end pts.).
- b) The (force) field can be written as a gradient of a scalar function, called "potential", traditionally written:

$$\vec{F} = -\nabla U$$
- c) $\nabla \times \vec{F} = 0$

(n.b., the three actually mean the same thing).

→
continued.

4

(iii) $\vec{F}(\vec{r}) = -\frac{k}{r^2} \hat{r}$ is given. We can show that \vec{F} is conservative in several different ways:

a) Note that \vec{F} is radial ("central"). Hence, $\vec{\nabla} \times \vec{F} = 0$.

b) We can also show a) directly. Rewrite \vec{F} :

$$\begin{aligned} \vec{F}(\vec{r}(x,y,z)) &= \vec{F}(x,y,z) = -\frac{k}{r^3} \vec{r}, \text{ using } \vec{r} = r \hat{r} \\ &= \frac{-k}{(x^2+y^2+z^2)^{3/2}} \cdot (x,y,z), \text{ using } r^2 = x^2+y^2+z^2 \\ &\quad \text{and } \vec{r} = (x,y,z). \end{aligned}$$

$$\text{Now, } \vec{\nabla} \times \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \frac{-kx}{(x^2+y^2+z^2)^{3/2}} & \frac{-ky}{(x^2+y^2+z^2)^{3/2}} & \frac{-kz}{(x^2+y^2+z^2)^{3/2}} \end{vmatrix}$$

$$= -k \hat{i} \left[\frac{z \partial}{\partial y} (x^2+y^2+z^2)^{-3/2} - y \frac{\partial}{\partial z} (x^2+y^2+z^2)^{-3/2} \right] + \dots$$

$$= -k \hat{i} \left[-\frac{3}{2} \cdot \frac{2zy}{(x^2+y^2+z^2)^{5/2}} + \frac{3}{2} \cdot \frac{2yz}{(x^2+y^2+z^2)^{5/2}} \right] + \dots$$

$$= 0 \hat{i} + 0 \hat{j} + 0 \hat{k} = \boxed{0} \quad \square$$

c) We can also show that $\exists U(r) \ni \vec{F} = -\vec{\nabla} U$:

$$\begin{aligned} \boxed{U(r) = -\frac{k}{r}} &\xrightarrow{\text{check}} -\vec{\nabla} U = -\frac{\partial U}{\partial r} \hat{r} \text{ (in spherical coordinates)} \\ &= -\frac{k}{r^2} \hat{r} = \vec{F} \quad \square \end{aligned}$$